

Characterization of Phosphate Glass Reinforced Gelatin Blend Bioactive Composite Films

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Abstract: Bioactive composite films were prepared using bioresorbable phosphate glass powder and biodegradable polymer gelatin (G) through solution casting process. Biocompatible monomer, 2-hydroxyethyl methacrylate (HEMA) was used as the cross-linking agent and bioresorbable phosphate glass (PG) powder was used as reinforcement filler. The composite films were obtained at various ratios of G, PG and HEMA. The PG modified gelatin composite (PG/G) film was fabricated at a weight ratio of 12:88 while HEMA modified gelatin composite (HEMA/G) film at 50:50 ratio. On the other hand, hybrid gelatin composite film, containing both PG and HEMA, was obtained using a G/PG/HEMA ratio of 44:12:44. Incorporation of PG improved the mechanical properties of the composite films. Morphological property of the composite films was investigated by stereo microscope and it revealed that the composite films were porous in nature. The thermal behaviour of the films was studied using thermogravimetric analysis. Water uptake of the films was also performed.

Keywords: Gelatin, phosphate glass, bioactive, composite films, stereo microscope.

1. INTRODUCTION

Bioresorbable composite has gained tremendous interest in the field of biomaterial research. Tissue engineering has brought new challenges in this field in terms of biodegradability, biocompatibility, homogeneity, osteoconductivity, vascularity, cell proliferation, controlled release, mechanical properties [1-3]. Both natural and synthetic polymers along with polylactic acid, polyglycolide, polycaprolactone and their copolymers, hydroxyapatite, calcium phosphate, hyaluronate and hyaluronate derivatives have been thoroughly studied to find a novel class of potential application in tissue engineering [4-6]. Polymer blending technique is simple and efficient to improve the properties of polymer up to a desired level and has been widely utilized in polymer modification field. It offers reduced processing cost and versatility in the selection of materials [7]. Polymer blending of compatible materials leads to substantial enhancement of mechanical and thermal performance [8-10]. A range of materials with different properties can be successfully blended to obtain fine tunable material for a particular application [11]. Various nano-reinforcement fillers such as silicate clay, carbon nanotubes,

graphene, calcium carbonate and phosphate glass are being extensively studied in the field of nanocomposites. These nano fillers are capable of enhancing the mechanical and thermal performance of the polymer [12]. Our present research aims at developing a biopolymer-organic-inorganic blend composite film with enhanced mechanical and thermal properties. In the present work, we chose phosphate based glass (20Na₂O-24CaO-16MgO-40P₂O₅) as a reinforcement filler because of its some important criteria regarding biomedical applications [13, 14]. The dissolution rate of the glass can be altered varying the composition to tailor the biomedical properties. The P₂O₅ provides the backbone structure of phosphate glass and has been evolved as a promising biomaterial [15, 16]. The organic phase of hard tissues contains type I collagen [17, 18]. Gelatin is a denatured collagen and possesses a wide range of biomedical properties making suitable for tissue engineering [19, 20]. In the present study, HEMA is used as a hydrophilic biocompatible monomer. HEMA is a hydrophilic monomer and is using in biomedical field [21]. Poly(HEMA) has also adequate biocompatibility and uses in medical science as implant [22]. The goal of this research work is to determine the influence of PG and HEMA on the preparation of a bio-artificial polymeric material using gelatin polymer that would be used as an excellent alternative to tissue scaffold material for artificial bone tissue engineering and drug delivery.

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2. EXPERIMENTAL

2.1. Materials

Gelatin (pharmaceutical grade) was collected from the Opsonin Pharma Limited, Bangladesh. Phosphate glass (molecular formula: $20\text{Na}_2\text{O}-24\text{CaO}-16\text{MgO}-40\text{P}_2\text{O}_5$) used in this study was supplied by the Department of Mechanical, Materials and Manufacturing Engineering, University of Nottingham, UK. Monomer HEMA (molecular weight: 130.14, melting point: $-12\text{ }^\circ\text{C}$, boiling point: $205\text{ }^\circ\text{C}$, miscible in water) was purchased from Fluka Chemie AG, CH-9470 Buchs.

2.2. Preparation of Blend Composite Films

Accurately weighed gelatin/phosphate glass/HEMA was dissolved in slightly hot water to form solution. The blending mixture was continuously stirred manually to aid formation of homogenous mixture and heated for about one and half an hour. The solution was finally cast on the plastic covered glass plate to form thin composite film. The solution layer was maintained into a thickness of about 0.50 mm on the glass plate. It was then dried in room temperature for about 48 hours. The dried composite films were peeled off and subjected to characterization studies. The composition of the materials studied is listed in the Table 1. Experimental flow diagram is presented in the Figure 1. Figures 2a-c depict the preparation of G/PG/HEMA blend solution by mechanical mixing, a composite film and sample prepared for test, respectively.

2.3. Mechanical Property of the Composite Films

Mechanical properties such as tensile strength (TS), tensile modulus (TM), and elongation at break (Eb%) of the films were investigated by the Universal Testing Machine (Hounsfield series S testing machine, H50 KS-0404) with a crosshead speed of 1 mm per second at a span distance of 25 mm. The dimensions of the test specimen were 60 mm \times 10 mm \times 0.02 mm. The experiment was carried out according to the European standard (ISO/DIS 527-1:2010).

2.4. Water Uptake (%) Profile of the Composite Films

The water uptake of the composite films was periodically (15, 30, 45, 60 sec) monitored up to 60 sec to find the water uptake nature of the composite films. Percentage water uptake was determined relative to the dry weight of the sample.

2.5. Thermal Characterization of the Composite Films

Various thermal properties like onset, offset and glass transition temperature of the samples were measured using thermo-mechanical analyzer (TMA) (Linseis TMA/DMA L77, USA). Figure 3b shows a TMA machine.

2.6. Morphological Characteristics of the Composite Film

The surface morphology of G/PG composite film was determined by stereo microscope (SM).

3. RESULTS AND DISCUSSIONS

The data presented in the manuscript are average values of at least five samples and the results obtained are within the accuracy of $\pm 1\%$.

3.1. Mechanical Analysis of the Composite Films

Tensile property is of great importance to find the suitability of diversified application of a polymeric material. The mechanical properties of the pure and composite gelatin films were tabulated in the Table 2. For each test, five samples were characterized. The values presented here is the average of five samples.

From the Table 2, it was observed that, incorporation of PG increased TS value while as TM value and Eb% were reduced. The TS, TM and Eb% of the pure gelatin were found to be 28 MPa, 846 MPa and 20%, respectively. On the other hand, for the G/PG composite film, the TS, TM and Eb% were obtained 36

Table 1: Composition (w/w %) of Different Composite Films

Composite Formulation	Gelatin (wt %)	Phosphate Glass (wt %)	HEMA (wt %)
G	100	0	0
G/PG	88	12	0
G/HEMA	50	0	50
G/PG/HEMA	44	12	44

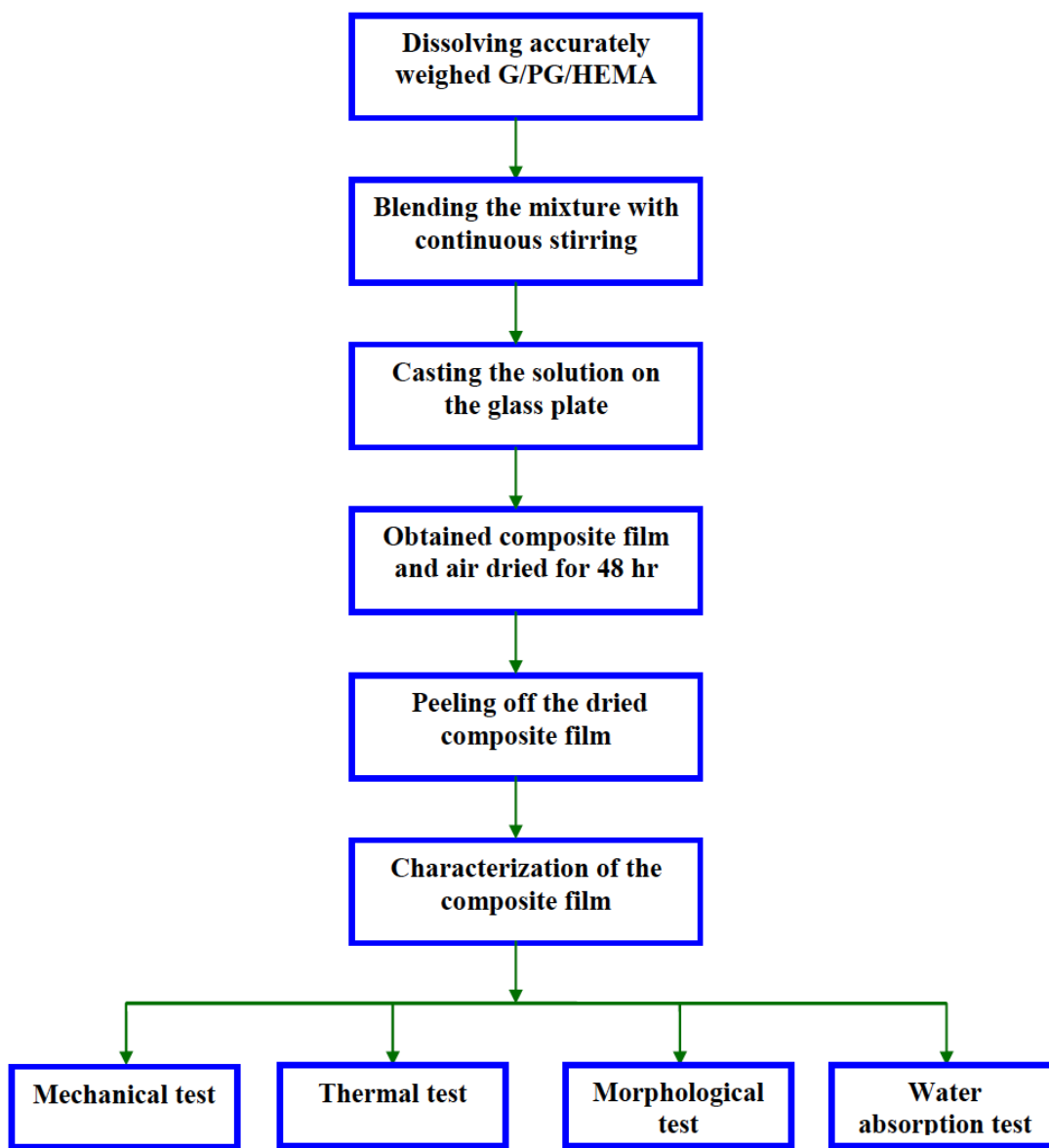


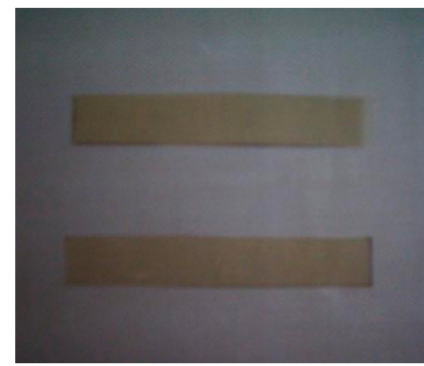
Figure 1: Experimental flow diagram.



(a)



(b)



(c)

Figure 2: (a): Preparation of G/PG/HEMA blend solution by mechanical mixing; 2 (b): A composite film; and 2 (c): Prepared sample for test.



Figure 3: (a): Universal Testing Machine; and (b): Thermo-mechanical Analyzer (TMA).

Table 2: Tensile Strength, Tensile Modulus and Elongation at Break (%) of Different Composite Films

Sample Name	Tensile Strength (MPa)	Tensile Modulus (MPa)	Elongation at Break (%)
G	28	846	20
G/PG	36	266	13
G/HEMA	31	62	156
G/PG/HEMA	19	36	120

MPa, 266 MPa and 13%, respectively. The improved TS may be due to the mechanical interlocking of the PG fillers with gelatin [23]. Moreover, metallic structure phosphate glass stiffens the gelatin film which increased TS value but reduced Eb%. Figures 4, 5 and 6 show the comparison of tensile strength, tensile modulus and elongation at break (%) among different composite films, respectively. Addition of PG improved 29% TS value (36 MPa) of G/PG composite film compared to pure gelatin film. Similarly, incorporation of HEMA increased TS and Eb% to 11% and 680%, respectively, with respect to pure gelatin film, but TM value was decreased to 62 MPa. HEMA imparts significant flexibility to the composite film. The increased of TS and Eb% may be due to the grafting or cross-linking of the HEMA molecules with gelatin polymer chain [24]. However, G/PG/HEMA composite film showed reduced TS and TM values which were 19 MPa and 36 MPa, respectively. Presence of HEMA disturbs the homogeneous distribution of PG into gelatin matrix and hence reduced mechanical interlocking promotes poor filler/matrix interaction. Similarly, PG imparts more water resistant P-O-P bonds reducing the availability of –OH groups in gelatin to interact with the –OH groups of HEMA [21]. These two phenomena may be

responsible to reduced mechanical properties when PG and HEMA are both present in the gelatin film. This study revealed that, introduction of both PG and HEMA into gelatin did not show any synergism effect on mechanical properties. Rather, PG incorporation provided improved tensile property.

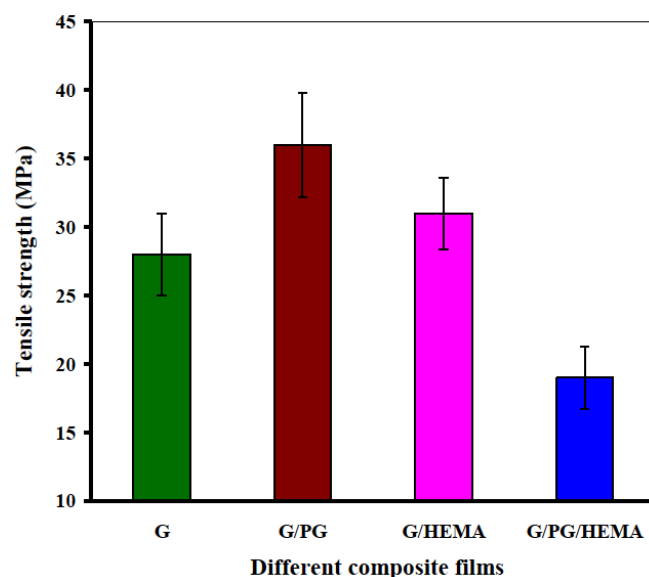


Figure 4: Comparison of tensile strength among different composite films.

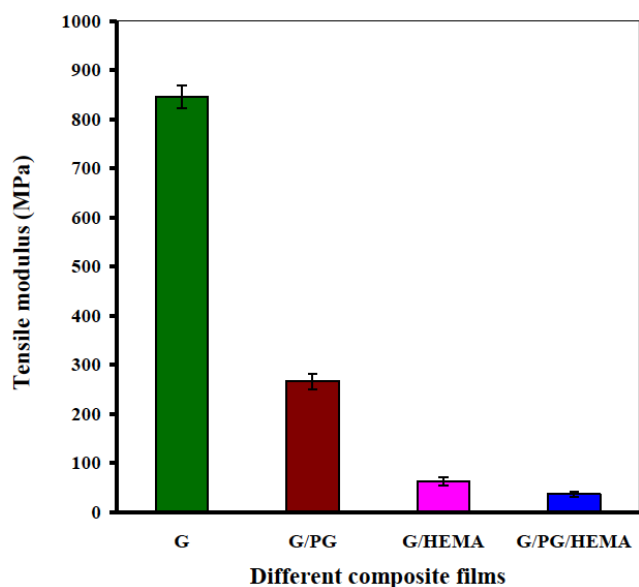


Figure 5: Comparison of tensile modulus among different composite films.

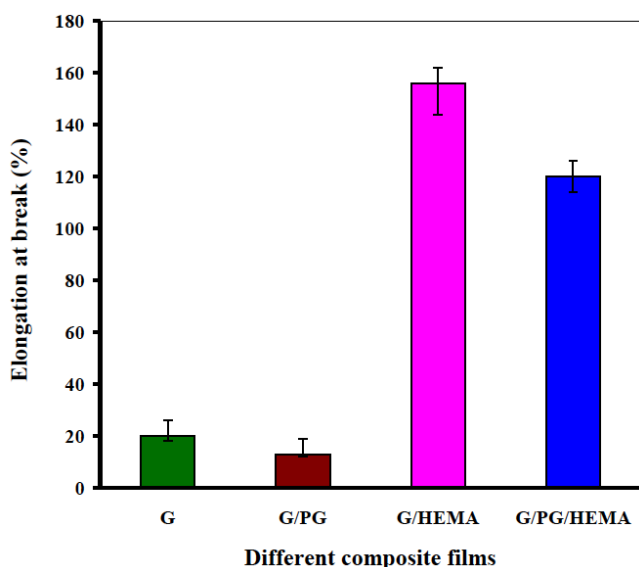


Figure 6: Comparison of elongation at break (%) among different composite films.

3.2. Investigation of Failure Modes by Stress–Strain Curves

To investigate the fracture modes of the prepared films, the stress–strain curves were studied. The strain–stress curves for G, G/PG, G/HEMA, and G/PG/HEMA based films are presented in Figure 7. Gelatin film exhibited intensive stress (56 N) within a few mm of strain (5 mm) which indicated the rigid nature of the film. Similarly, addition of phosphate glass in gelatin film showed more stiffness. After 3 mm of strain, G/PG films reached to 76 N of stress. Addition of PG in the gelatin film is clearly revealed that gelatin film

was successfully reinforced with PG powder during casting process. Both gelatin and phosphate glass reinforced gelatin films showed sharp peaks and indicated very low elongation of break that was described in Figure 6. On the other hand, HEMA treated gelatin (G/HEMA) film showed the maximum stress (62 N) after 30 mm of strain then film fractured at 40 mm. Similarly, the film G/PG/HEMA exhibited a long strain (30 mm) and but less stress (42 N). From this investigation, this is clear that phosphate glass powder acted as a good reinforcing agent and HEMA monomer provided flexibility to the films. Similar type of stress–strain observations are reported elsewhere [25]. It is to be mentioned that polymers are classified into three types according to the type of stress–strain curves. In brittle polymers such as polystyrene, the stress–strain curves are linear up to the fracture point. Here, G and G/PG exhibited brittle nature. Tough polymers such as polyethylene exhibit a yield point followed by extensive elongation at almost constant stress. The films of G/HEMA and G/PG/HEMA showed the nature of tough polymer like polyethylene. The third type of stress–strain curve is exhibited by elastomers such as polyurethane, in which a nonlinear curve up to break point, and the elongation percentage may be of the order of several hundred percent [25].

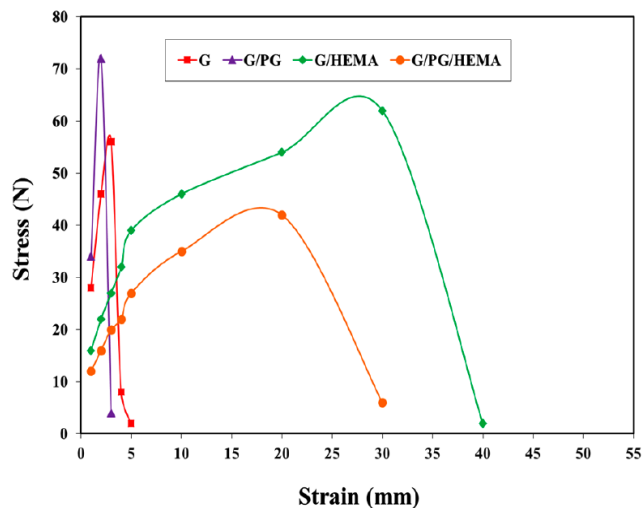


Figure 7: Stress-strain curve of Gelatin (G), Gelatin-Phosphate Glass (G/PG), Gelatin-HEMA and Gelatin-Phosphate Glass-HEMA (G/PG/HEMA).

3.3. Thermal Analysis (TMA) of the Composite Films

The glass transition temperature (T_g) was investigated by thermomechanical analysis. Figure 8 shows T_g of the different composite films. The highest T_g was obtained for G/PG composite film.

Table 3: Thermal Properties of Different Composite Films

Sample Name	Onset Temperature (°C)	Glass Point (°C)	Offset Temperature (°C)
G	40.8	44.9	50.4
G/PG	66.1	66.2	69.7
G/HEMA	31.6	32.6	37.0
G/PG/HEMA	36.0	38.7	43.5

The glass transition point of pure gelatin was found 44.9°C whereas it was 32.6°C for G/HEMA, 66.2°C for G/PG and 38.7°C for G/PG/HEMA composite films. The changed in morphology as well as better filler-matrix interaction might have changed the T_g .

From the Table 3, it is seen that the G/PG composite film showed the highest onset, offset and glass transition value. The incorporation of fillers usually increased T_g of the composites. The improved T_g may be ascribed due to the restriction of mobility of the polymer chain resulted from the better filler-matrix interaction [26, 27].

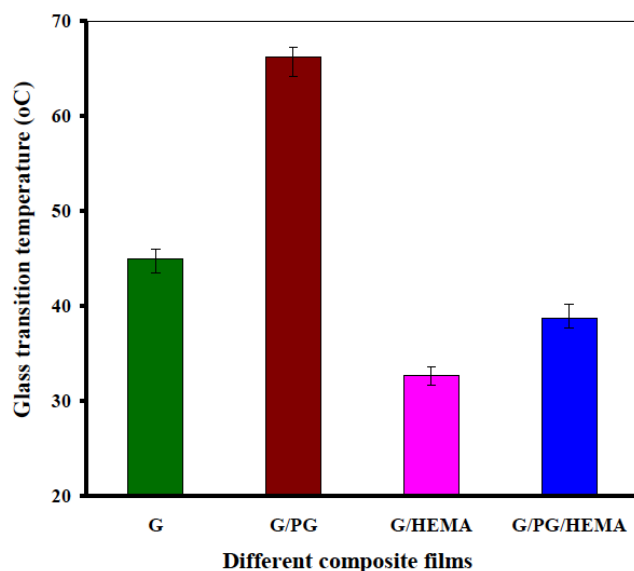


Figure 8: Comparison of glass transition temperature (T_g) among different composite films.

3.4. Water Uptake (%) Characteristics of the Composite Films

The samples were immersed into deionized water for a set period of time. The samples were then removed from water after set time interval and their wet weight were measured immediately after tenderly wiping their surfaces. The amount of water uptake was calculated dividing weight difference between the wet and dry sample by the weight of dry sample. Water

absorption of the composite films against total soaking time (sec) was presented in the Figure 9. The maximum water uptake was observed for pure gelatin film, as expected, due to the presence of higher amount of hydrophilic -OH groups. The G/PG composite films had moderately water uptake reaching value 4% after 60 sec soaking time. Incorporation of phosphate glass induces more water resistant P-O-P bonds which reduces the strong hydrophilic nature of gelatin [28]. A slight lower water uptake was shown by the G/PG/HEMA composite films compared to G/PG film. This may be due to the presence of cross-linking [29] and water resistant P-O-P bonds as well as lesser amount of -OH groups.

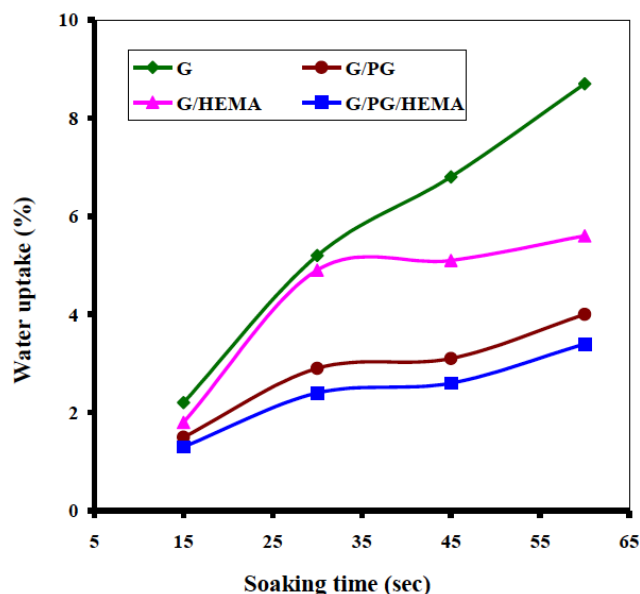


Figure 9: Percentage water uptake of the different composite films against soaking time (sec).

3.5. Morphology of the Composite Films

The pore morphology of the G/PG composite films was studied using stereo microscope. The stereo micrograph of the G/PG composite film was presented in the Figure 10. A dissimilar vascular shape pore structures was observed in the composite film. The distribution of pores was not uniform. Presence of

phosphate glass was responsible to create these pores in the composite film. The distribution nature of PG inside the gelatin polymer matrix demonstrates low dispersion quality. Cluster size pores inside the bulk sample may be due to the high loading percentage of PG (12 wt %) into the gelatin matrix.

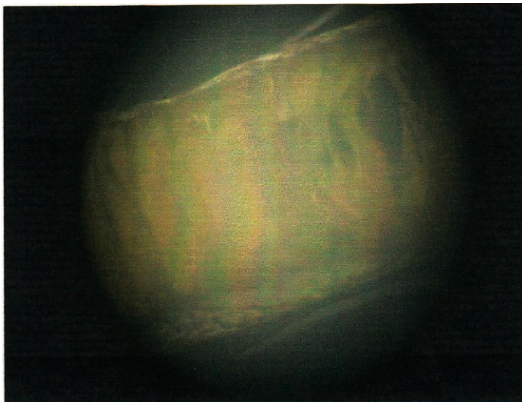


Figure 10: Stereo micrograph of the G/PG composite film.

4. CONCLUSION

Gelatin and phosphate glass based biocomposite films were developed using biopolymer, gelatin and bioresorbable phosphate glass powder. The incorporation of phosphate glass into gelatin showed improved tensile and thermal properties. Stereo micrograph revealed porous structures of the composite films. Moreover, the degradation behavior of the composite films can be controlled by changing the amount of phosphate glass powders. The fabricated porous bio-composite films have the potential to be used in biomedical and tissue engineering applications.

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